

# RELIABILITY OF LEAD-FREE SOLDERS FOR DIE ATTACH IN AUTOMOTIVE POWER MODULES

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based on a presentation at EPTC 2022 in Singapore [\*]

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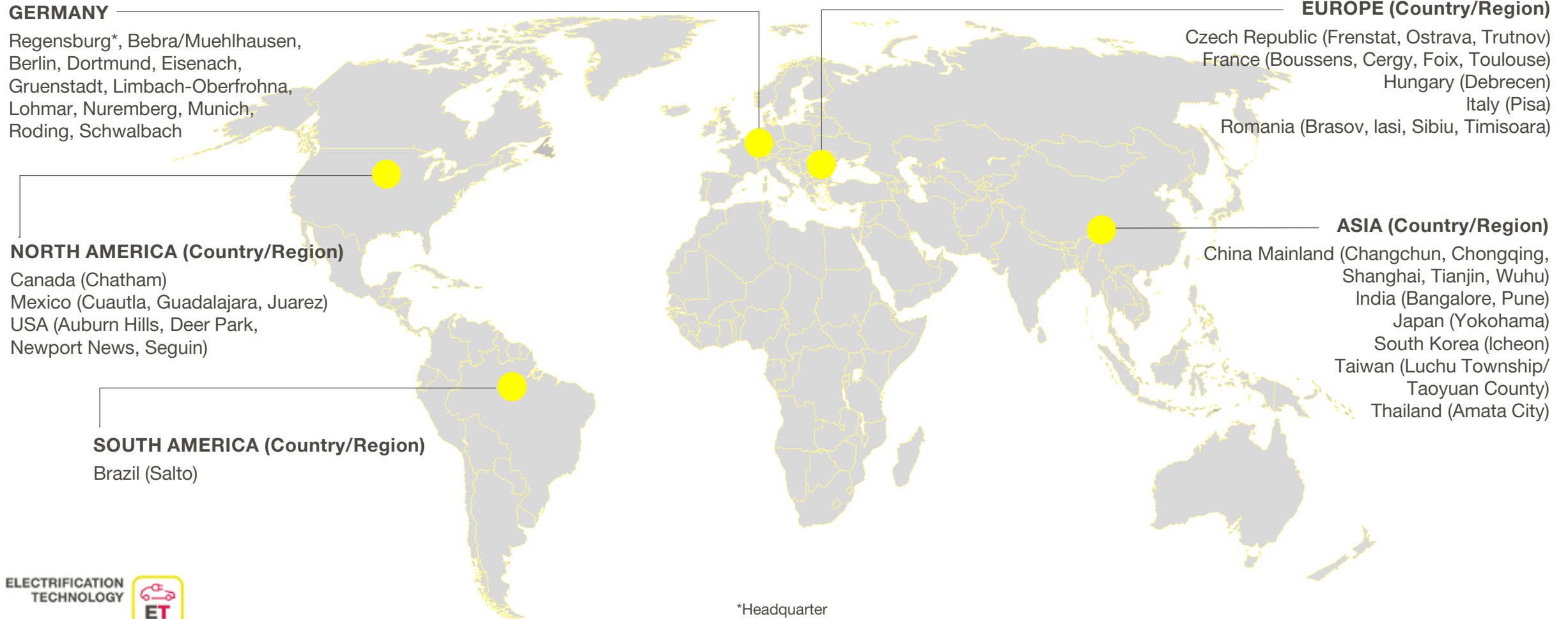
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OUR VISION

# GLOBAL FOOTPRINT



# AGENDA

1 INTRODUCTION

2 METHODS

3 RESULTS AND DISCUSSION

4 SUMMARY

5 OUTLOOK

# INTRODUCTION – POWER MODULE

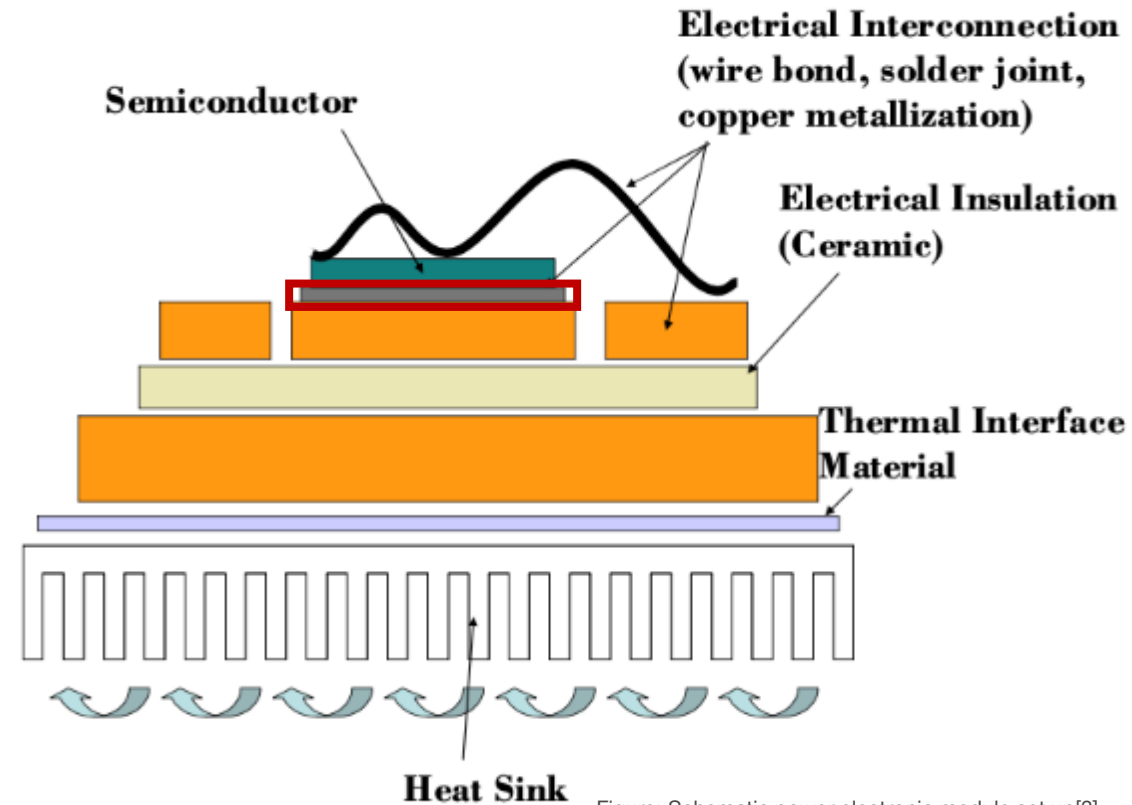


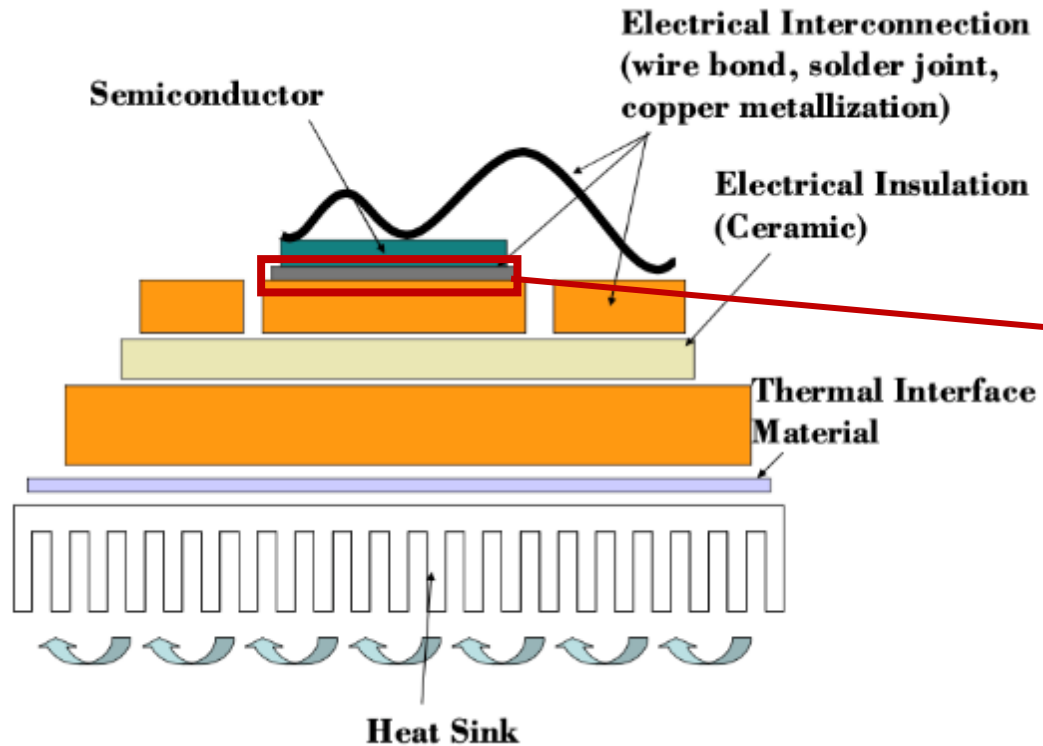
Figure: Schematic power electronic module set up[3]



Comparison of four Sn-based die attach materials during active power cycling under equal conditions

[3] Egelkraut, S., et al., "Evolution of Shear Strength and Microstructure of Die Bonding Technologies for High Temperature Applications during Thermal Aging," *12<sup>th</sup> Electronic Packaging Technology Conference* (2010)  
Bettina Ottinger, Sebastian Koenig

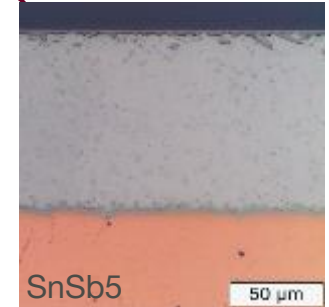
# INTRODUCTION – POWER MODULE



- SAC305
- SnSb5
- SnSb10
- PFDS400®

## Bulk alloyed solder materials:

- Sn-based solder alloy with additives like Ag, Cu or Sb
- Intermetallic compound (IMC) layer at the interfaces → metallic bond



## Layered diffusion solder materials:

- Layered structure of Sn-based solder alloy and Cu
- Growth of IMC over the entire Sn-alloy-layer

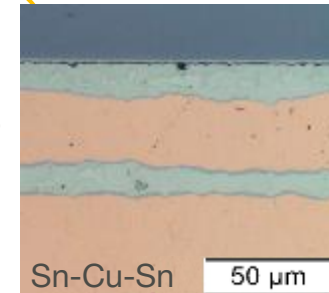


Figure: Schematic power electronic module set up[3]



Comparison of four Sn-based die attach materials during active power cycling under equal conditions

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# METHODS - ACTIVE POWER CYCLING TEST



## Design of the active power cycling test:

- Based on the ECPE Guideline 324 (AQG 324) [5]
- Applying a constant load current of about 250 A
- Temperature swing  $\Delta T = 100\text{K}$  ( $T_{\min} = 40\text{ }^{\circ}\text{C}$  and  $T_{\max} = 140\text{ }^{\circ}\text{C}$ )
- Duration of each cycle  $t_{\text{on}} = 3\text{s}$  and  $t_{\text{off}} = 6\text{s}$

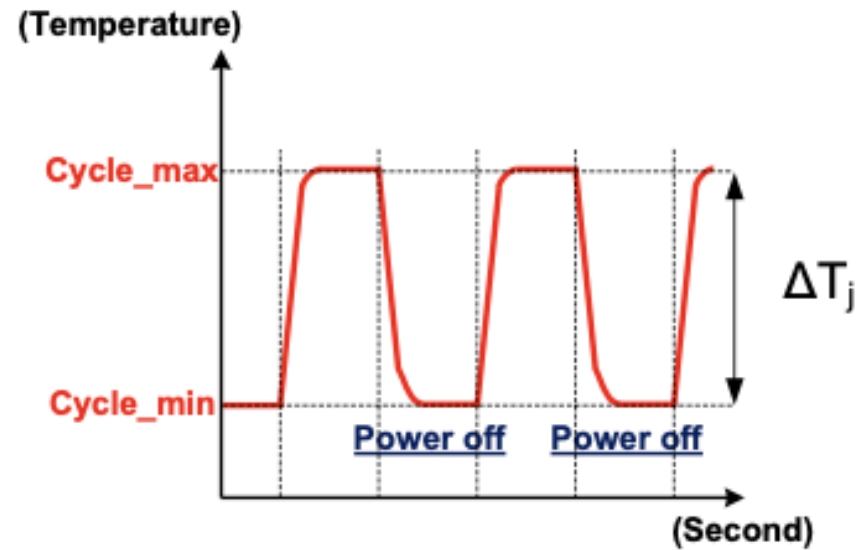


Figure: Schematic junction temperature history [4]

[4] Liao, L. et al., "Power cycling test and failure mode analysis of high-power module," *ICEP Proceedings* (2016), pp. 372-377

[5] Automotive AQG 324, "<https://www.ecpe.org/index.php?elD=dumpFile&t=f&f=23930&token=ab9f61d08229d223b108cb44f00aa4db948ad4e4>" (Accessed: september 20, 2022)



# METHODS - QUALITY OF THE DIE ATTACH

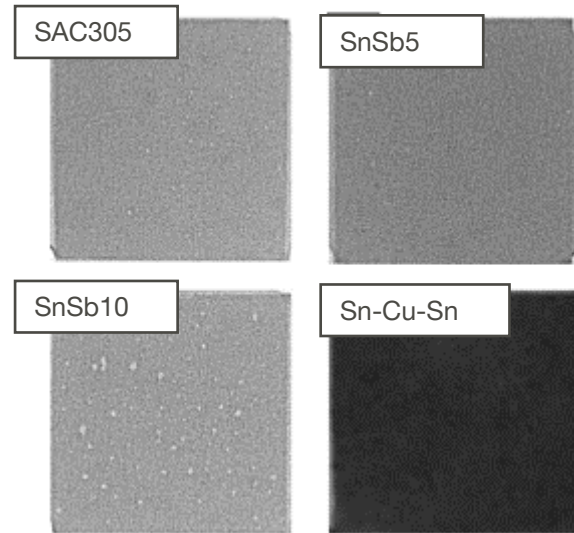


Figure: Image of X-ray or SAM analysis

Solder material	Ratio of the maximum void area %
SAC305	0.03
SnSb5	0.03
SnSb10	0.17
Sn-Cu-Sn	0.01

} < 5%



Quality of the soldered die interconnection via X-ray analysis or SAM analysis:

- Measuring the local maximum void of each die
- Calculation of the maximum void area ratio over the total die surface

→ All soldered die attaches are lower than the limited maximum void area ratio of (5-10%) [6]

[6] Chang, J. et al., "Finite Element Modeling Predicts the Effect of Voids on Thermal Shock Reliability and Thermal Resistance of Power Devices." *Welding Journal* (2006), pp. 63 -70

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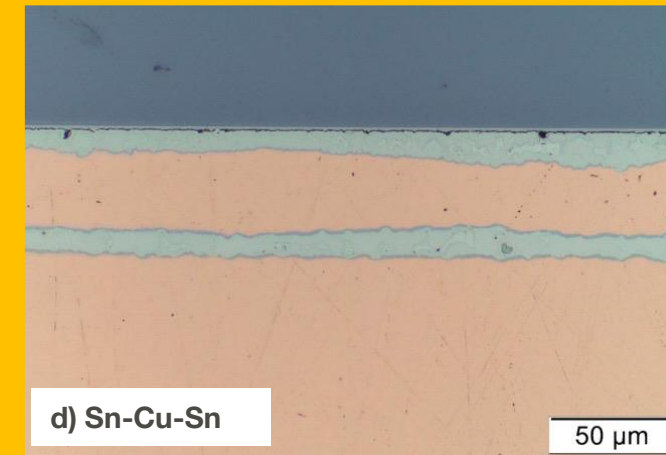
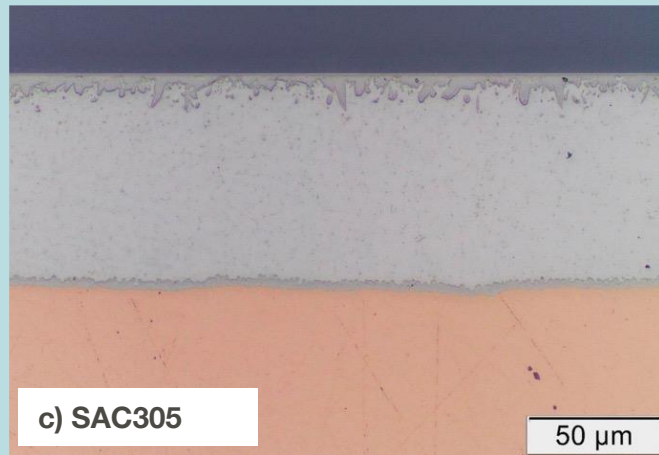
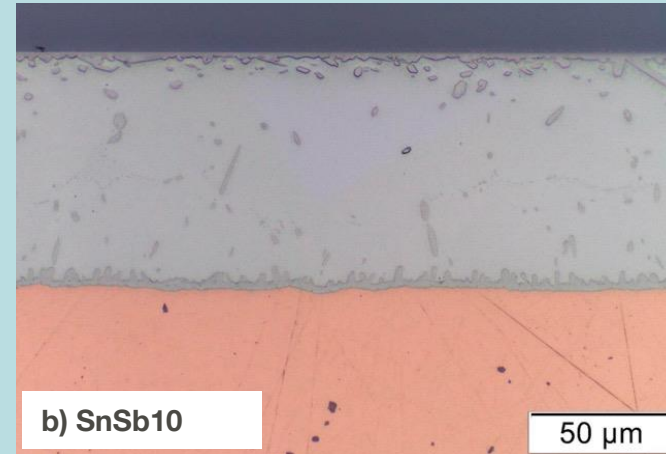
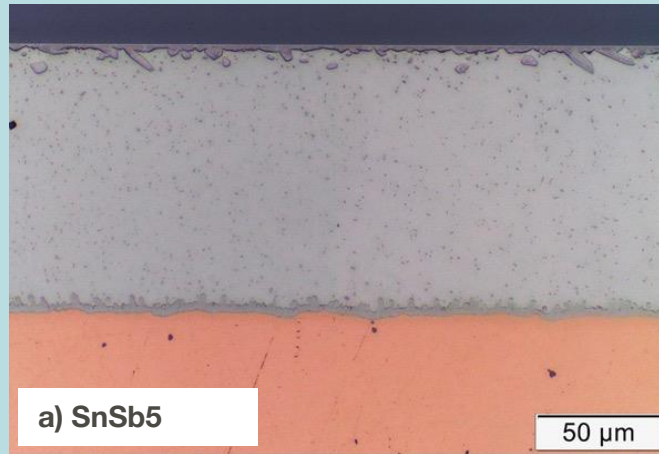
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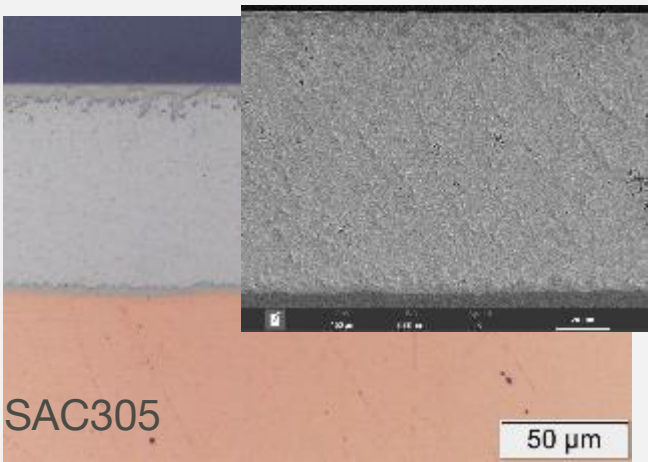
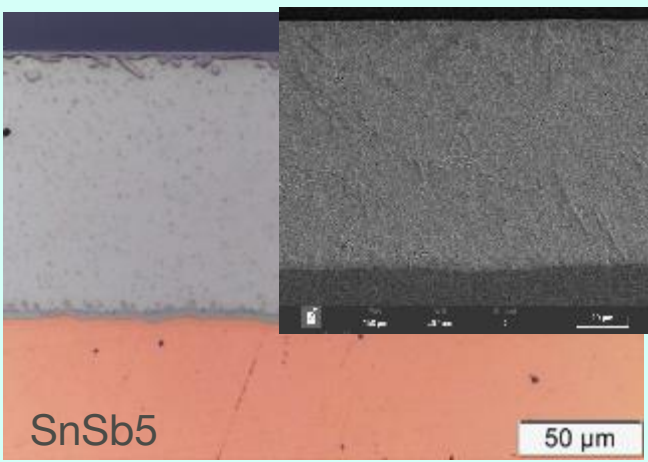
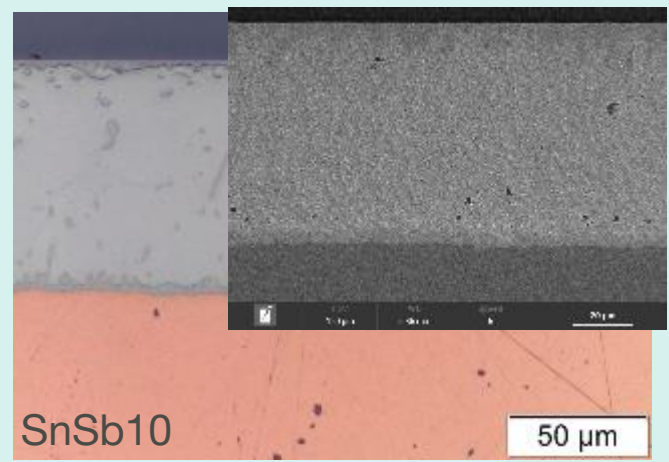

# RESULTS - INITIAL MICROSTRUCTURE

Bulk alloyed solder materials

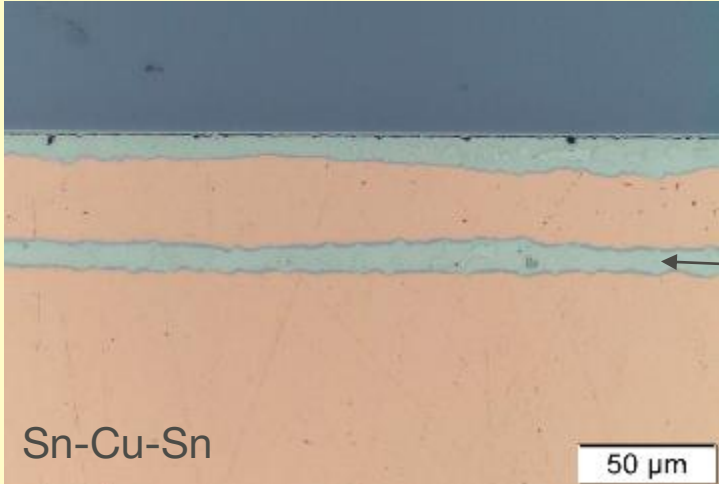


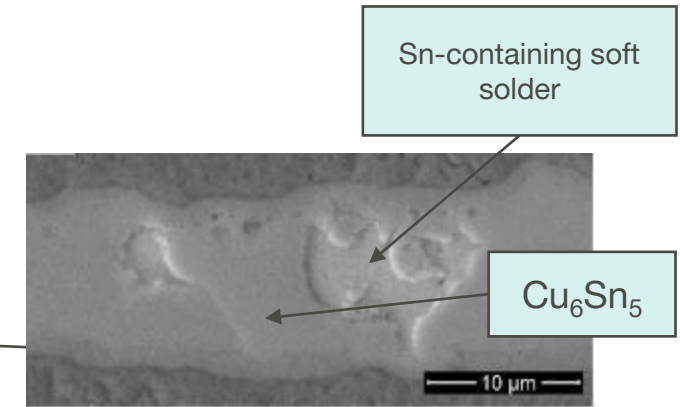
Layered diffusion solder materials

# RESULTS - INITIAL MICROSTRUCTURE

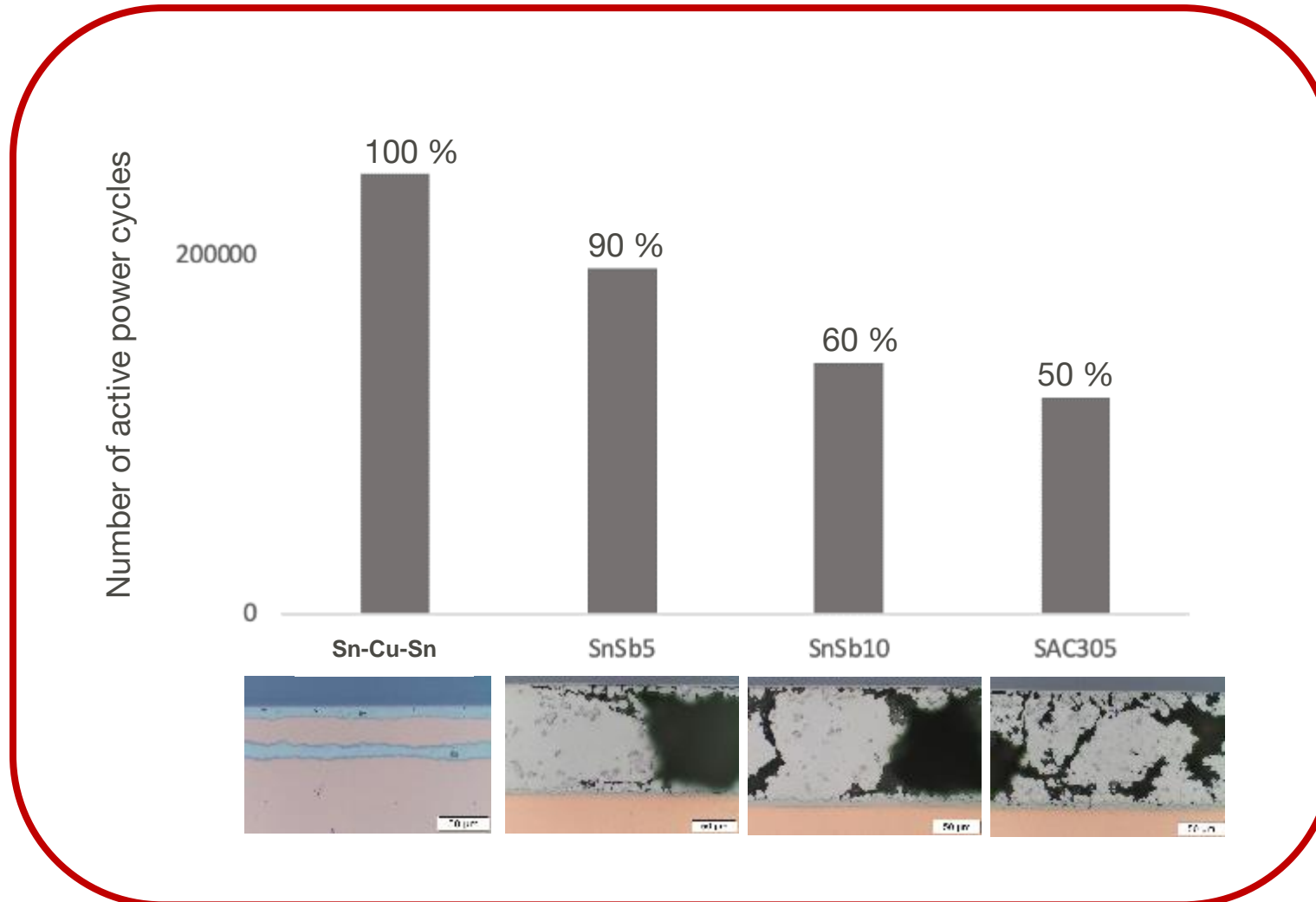
Bulk alloyed solder materials	 <p>SAC305</p> <p>50 µm</p>	 <p>SnSb5</p> <p>50 µm</p>	 <p>SnSb10</p> <p>50 µm</p>
<b>Basic microstructure of the bulk solder</b>	<ul style="list-style-type: none"> <li>• Fine and homogeneous microstructure of the bulk solder</li> </ul>	<ul style="list-style-type: none"> <li>• Solidified solder structures</li> <li>• Homogeneous microstructure of the bulk solder</li> </ul>	 <p>50 µm</p>
<b>IMC at the interfaces</b>	<ul style="list-style-type: none"> <li>• Homogenous and needle-like crystalline structure of the IMC <math>\text{Cu}_6\text{Sn}_5</math> layer</li> <li>• 2-3 µm thickness of <math>\text{Cu}_6\text{Sn}_5</math> IMC layer</li> </ul>	<ul style="list-style-type: none"> <li>• Homogenous and needle-like crystalline structure of the IMC <math>\text{Cu}_6\text{Sn}_5</math> layer</li> <li>• 2-3 µm thickness of <math>\text{Cu}_6\text{Sn}_5</math> IMC layer</li> </ul>	<ul style="list-style-type: none"> <li>• Homogenous and needle-like crystalline structure of the IMC <math>\text{Cu}_6\text{Sn}_5</math> layer</li> <li>• 2-3 µm thickness of <math>\text{Cu}_6\text{Sn}_5</math> IMC layer</li> </ul> <p>50 µm</p>

# RESULTS - INITIAL MICROSTRUCTURE

<p><b>Layered diffusion solder materials</b></p>	 <p>Sn-Cu-Sn</p> <p>50 μm</p>
<p><b>Basic microstructure bulk solder</b></p>	<ul style="list-style-type: none"> <li>• Layered structure</li> <li>• Sn-layer is transformed into <math>\text{Cu}_6\text{Sn}_5</math> (columns) with “Sn-islands” in the middle of the Sn-solder layer</li> <li>• Thickness of copper layer remains constant</li> </ul>
<p><b>IMC at the interface</b></p>	<ul style="list-style-type: none"> <li>• Column-structure of <math>\text{Cu}_6\text{Sn}_5</math> over the entire Sn-solder layer → connecting the interfaces</li> <li>• At the interface of Cu and Sn the IMC <math>\text{Cu}_3\text{Sn}</math> can be detected</li> </ul>

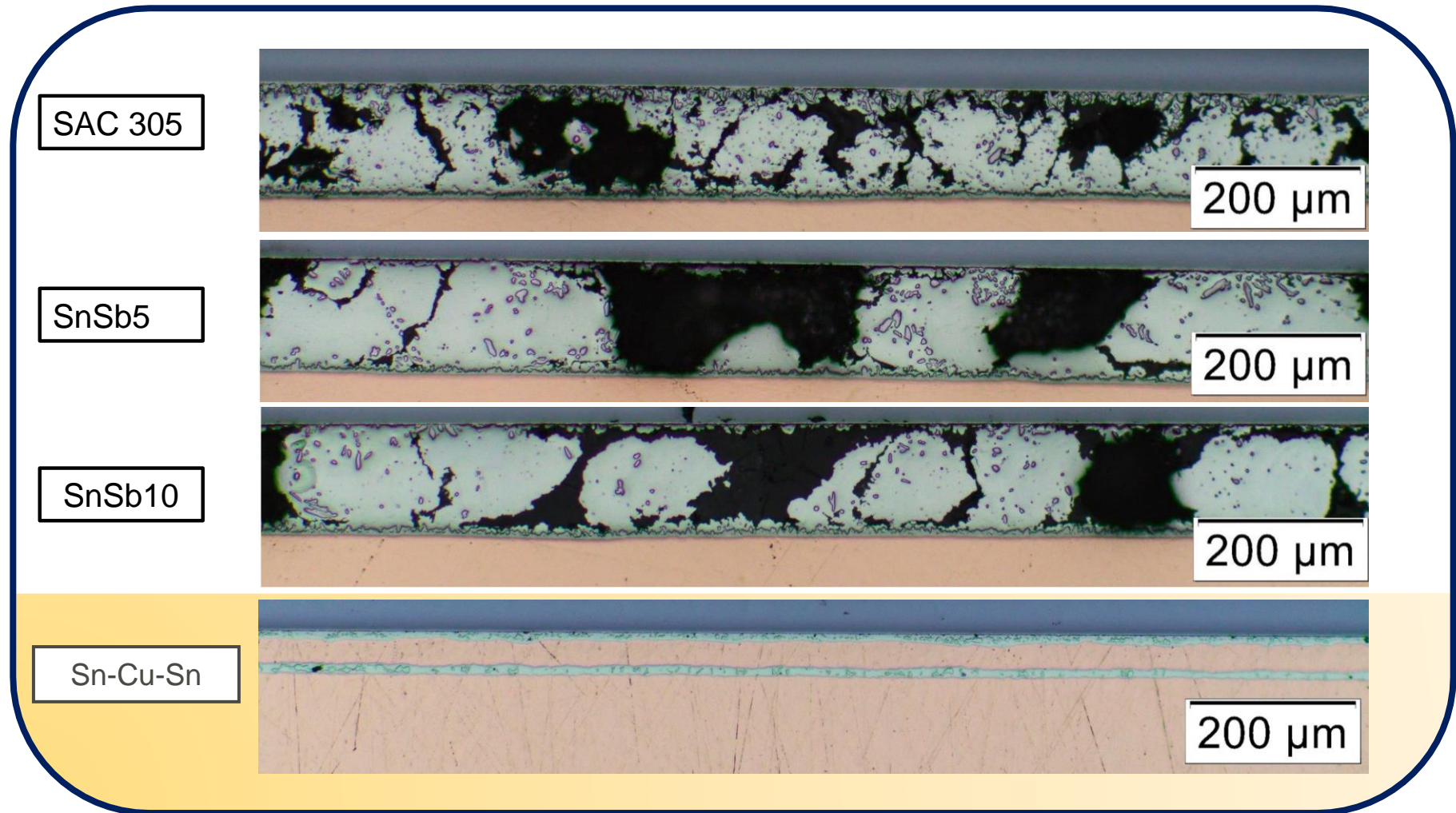


# RESULTS - ACTIVE POWER CYCLING TEST

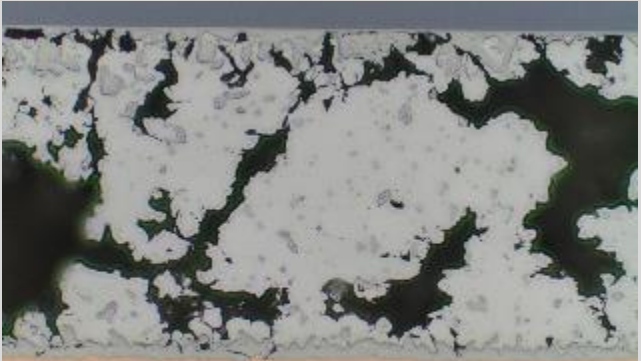
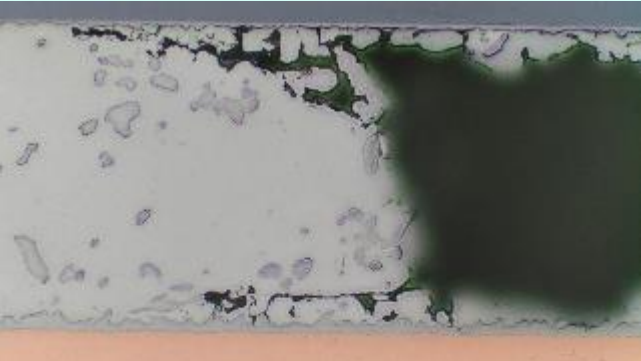
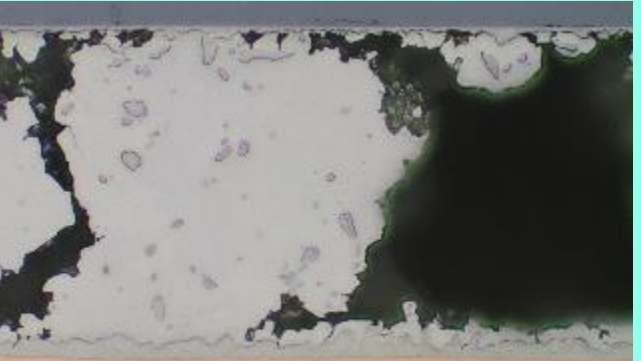


**50 % higher lifetime with layered diffusion solder material Sn-Cu-Sn compared to SAC305**

# RESULTS - MICROSTRUCTURE AFTER POWER CYCLING

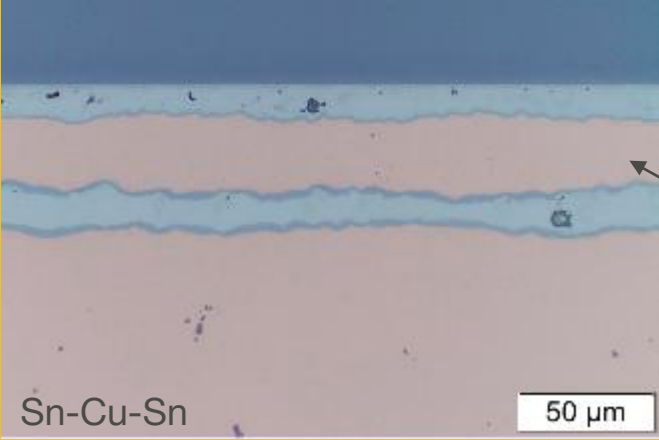


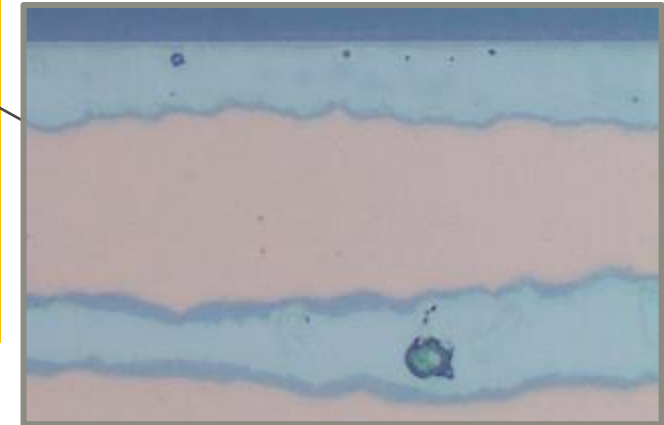
# RESULTS - MICROSTRUCTURE AFTER POWER CYCLING

<p><b>Bulk alloyed solder materials</b></p>	 <p>SAC305 <span style="float: right;">50 μm</span></p>	 <p>SnSb5 <span style="float: right;">50 μm</span></p>	 <p>SnSb10 <span style="float: right;">50 μm</span></p>
<p><b>Basic microstructure bulk solder</b></p>	<ul style="list-style-type: none"> <li>• Coarsening of the microstructure</li> <li>• <math>\text{Cu}_6\text{Sn}_5</math> IMC in the middle of the solder layer</li> <li>• Defect zones over the entire solder</li> <li>• Crack initiation inside the bulk solder</li> </ul>	<ul style="list-style-type: none"> <li>• Coarsening of the microstructure</li> <li>• <math>\text{Cu}_6\text{Sn}_5</math> IMC in the middle of the solder layer</li> <li>• Large local defect zones</li> <li>• Crack initiation inside the bulk solder</li> </ul>	<ul style="list-style-type: none"> <li>• Coarsening of the microstructure</li> <li>• <math>\text{Cu}_6\text{Sn}_5</math> IMC in the middle of the solder layer</li> <li>• Blocky phases couldn't be detected → Large local defect zones</li> <li>• Crack initiation inside the bulk solder</li> </ul>
<p><b>IMC at the interfaces</b></p>	<ul style="list-style-type: none"> <li>• Levelled needle-like crystalline structure at the IMC</li> </ul>	<ul style="list-style-type: none"> <li>• Levelled needle-like crystalline structure at the IMC</li> </ul>	<ul style="list-style-type: none"> <li>• Levelled needle-like crystalline structure at the IMC</li> </ul>

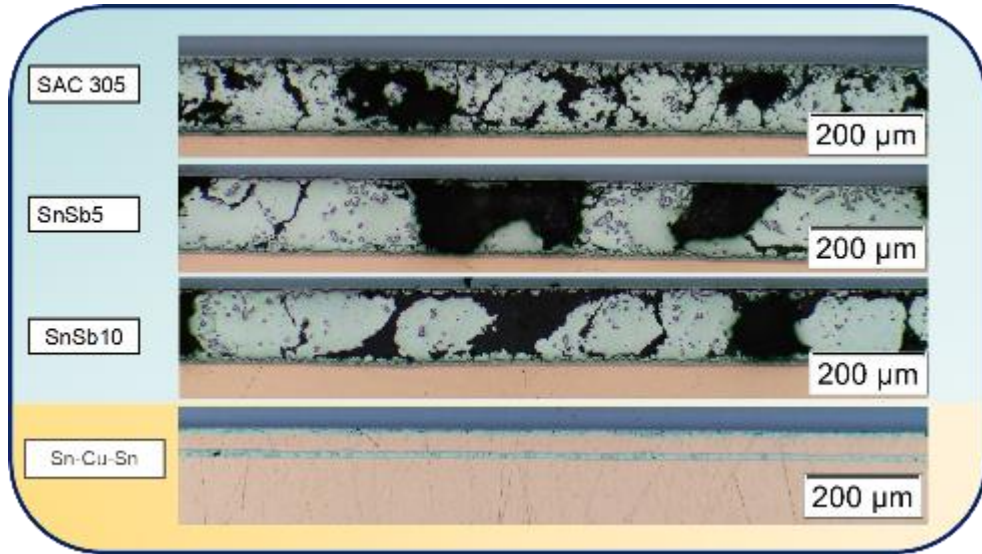


# RESULTS - MICROSTRUCTURE AFTER POWER CYCLING

<b>Layered diffusion solder materials</b>	 <p>Sn-Cu-Sn</p> <p>50 µm</p>
<b>Basic microstructure bulk solder</b>	<ul style="list-style-type: none"><li>• Layered structure</li><li>• <math>\text{Cu}_6\text{Sn}_5</math> columns over the entire Sn-layer</li><li>• Reduced amount of "Sn island" thickness of copper layer remains constant</li><li>• No defects visible</li></ul>
<b>IMC at the interface</b>	<ul style="list-style-type: none"><li>• Increase of the column-structure <math>\text{Cu}_6\text{Sn}_5</math> connecting the interfaces</li><li>• Increase of the <math>\text{Cu}_3\text{Sn}</math> intermetallic compound at the interface of Cu and Sn</li></ul>



# DISCUSSION



The bulk alloyed solders SAC 305, SnSb5 and SnSb10:

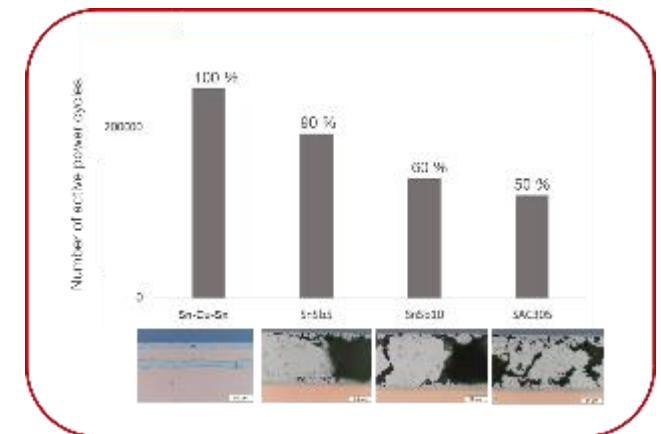
- Strong metallic bond at the interfaces with  $\text{Cu}_6\text{Sn}_5$
- Growth of IMC in the the solder layer → crack initiation
- Higher homologous temperature at  $T_{\text{max}}=140\text{ °C}$  indicates earlier material fatigue

The layered diffusion solder (Sn-Cu-Sn):

- Strong metallic bond at the interfaces with  $\text{Cu}_3\text{Sn}$  and  $\text{Cu}_6\text{Sn}_5$
- $\text{Cu}_6\text{Sn}_5$  columns over the entire Sn-solder layer stabilized and hardened the die attach against thermo-mechanical stress

Table: Material properties [7,8]:

Solder	SAC 305	SnSb5	SnSb10	$\text{Cu}_6\text{Sn}_5$	$\text{Cu}_3\text{Sn}$	Cu	Sn
Melting temperature $T_m$	217 °C	240 °C	250 °C	415 °C	676 °C	1085 °C	232 °C
Homologous temperature at 140 °C	0,64	0,58	0,56	0,34	0,21	0,13	0,60
CTE ppm/K	21	27	/	16,3	18,2 – 19,0	17,3	21



[7] Ehrhardt, Christian, Matthias Hutter, Constanze Weber, and Klaus-Dieter Lang. "Active Power Cycling Using Copper Tin TLPB Joints as New Die-Attach Technology," *PCIM Europe Nuremberg*, Germany, 19-21 May 2015, pp. 1268-1275

[8] Syed-Khaja, Aarif. "Diffusion Soldering for the High-Temperature Packaging of Power Electronics," FAU University Press (2018), pp. 31-33

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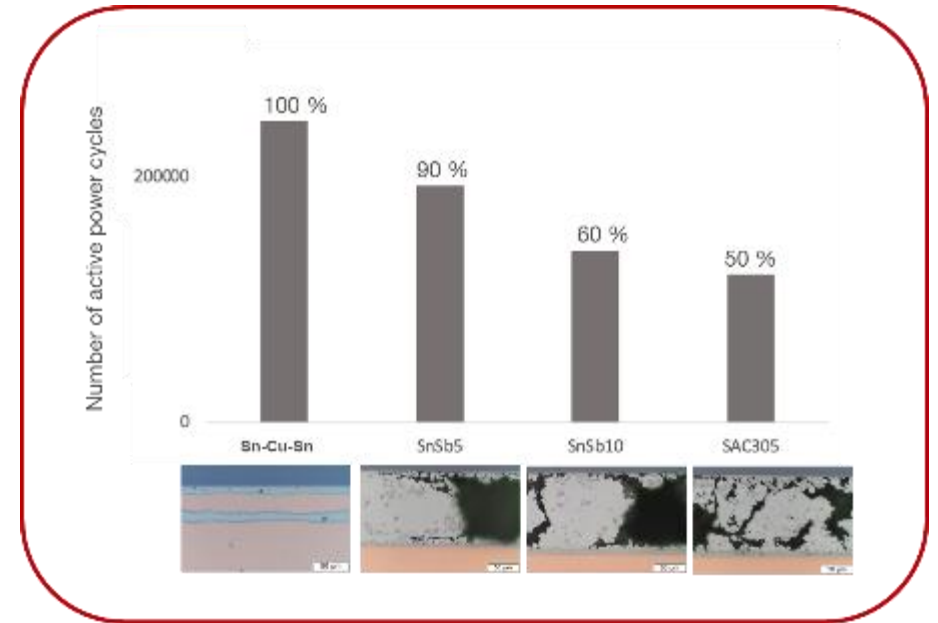
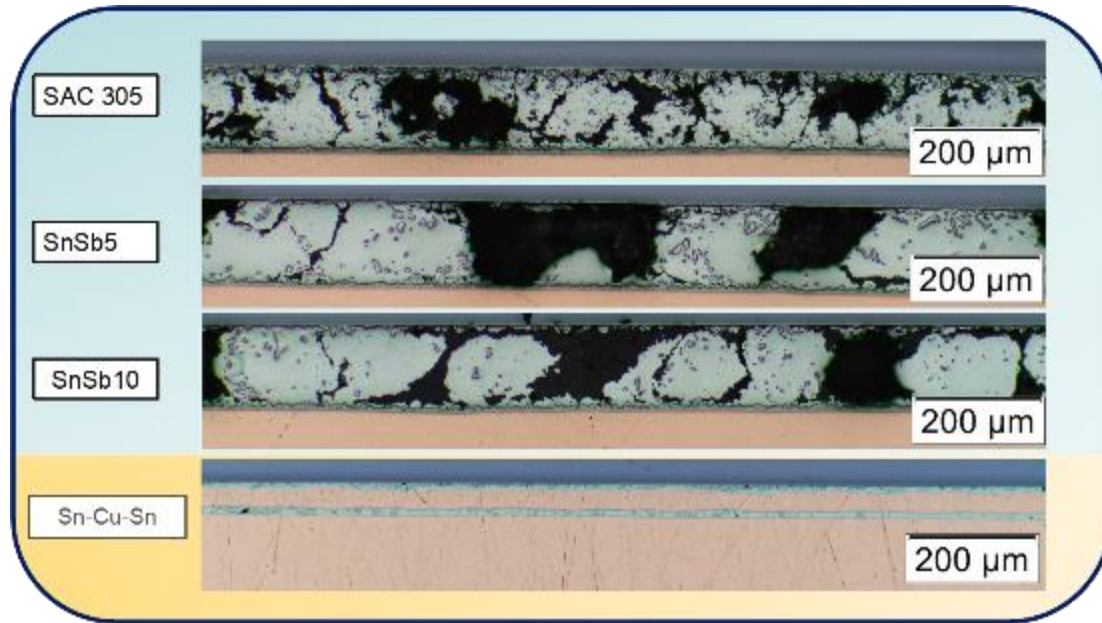
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# SUMMARY



 **50 % higher lifetime with layered diffusion solder material PFDS400®**

# SUMMARY

- DOE study has been performed on the power module
- A slight increase of maximum principal stresses is observed when increasing with IMP thickness - stresses are not critical
- Cyclic equivalent plastic strain decreases with increase in IMP thickness – low chances of die attach failure
- Von Mises stresses on metallization layer at die attach interface – not critical
- Higher the IMP thickness tends to have higher the lifetime of the power module with respect to die attach

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# OUTLOOK

- Further investigations are planned with improved topside connection on SiC dies
- Additional FEM analysis will provide further insight in lifetime potential of TLPS layers
- Geometrical stress optimization will be supported by FEM
- Activities will be supported by FHG ENAS